

# Fully Integrated, Hall-Effect-Based Linear Current Sensor IC with 2.1 kV<sub>RMS</sub> Isolation and Low-Resistance Current Conductor

### **FEATURES AND BENEFITS**

- Low-noise analog signal path
- Device bandwidth is set via the new FILTER pin
- 5 μs output rise time in response to step input current
- 80 kHz bandwidth
- Total output error 1.5% at  $T_A = 25$ °C
- Small footprint, low-profile SOIC8 package
- 1.2 mΩ internal conductor resistance
- 2.1 kV<sub>RMS</sub> minimum isolation voltage from pins 1-4 to pins 5-8
- 5.0 V, single supply operation
- 133 to 185 mV/A output sensitivity
- Output voltage proportional to DC currents
- Factory-trimmed for accuracy
- Extremely stable output offset voltage
- · Nearly zero magnetic hysteresis
- Ratiometric output from supply voltage



PACKAGE: 8-Lead SOIC (suffix LC)



Not to scale

### DESCRIPTION

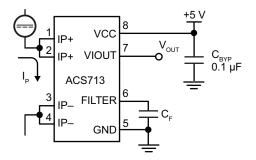
The Allegro™ ACS713 provides economical and precise solutions for DC current sensing in industrial, commercial, and communications systems. The device package allows for easy implementation by the customer. Typical applications include motor control, load detection and management, switch-mode power supplies, and overcurrent fault protection. The device is not intended for automotive applications.

The device consists of a precise, low-offset, linear Hall circuit with a copper conduction path located near the surface of the die. Applied current flowing through this copper conduction path generates a magnetic field which the Hall IC converts into a proportional voltage. Device accuracy is optimized through the close proximity of the magnetic signal to the Hall transducer. A precise, proportional voltage is provided by the low-offset, chopper-stabilized BiCMOS Hall IC, which is programmed for accuracy after packaging.

The output of the device has a positive slope ( $>V_{IOUT(Q)}$ ) when an increasing current flows through the primary copper conduction path (from pins 1 and 2, to pins 3 and 4), which is the path used for current sampling. The internal resistance of this conductive path is 1.2 m $\Omega$  typical, providing low power loss. The thickness of the copper conductor allows survival of

Continued on the next page...

## **Typical Application**



Application 1. The ACS713 outputs an analog signal,  $V_{OUT}$ . that varies linearly with the unidirectional DC primary sampled current,  $I_P$ , within the range specified.  $C_F$  is recommended for noise management, with values that depend on the application.

# Fully Integrated, Hall-Effect-Based Linear Current Sensor IC with 2.1 $kV_{RMS}$ Isolation and Low-Resistance Current Conductor

### **DESCRIPTION** (continued)

the device at up to  $5\times$  overcurrent conditions. The terminals of the conductive path are electrically isolated from the signal leads (pins 5 through 8). This allows the ACS713 to be used in applications requiring electrical isolation without the use of opto-isolators or other costly isolation techniques.

The ACS713 is provided in a small, surface mount SOIC8 package. The leadframe is plated with 100% matte tin, which is compatible with standard lead (Pb) free printed circuit board assembly processes. Internally, the device is Pb-free, except for flip-chip high-temperature Pb-based solder balls, currently exempt from RoHS. The device is fully calibrated prior to shipment from the factory.

#### **SELECTION GUIDE**

Part Number	Packing*	T <sub>A</sub> (°C)	Current Sensing Range, I <sub>P</sub> (A)	Sensitivity, Sens (Typ) (mV/A)
ACS713ELCTR-20A-T	Tape and reel, 3000 pieces/reel	-40 to 85	0 to 20	185
ACS713ELCTR-30A-T	Tape and reel, 3000 pieces/reel	-40 to 85	0 to 30	133

<sup>\*</sup>Contact Allegro for additional packing options.

### **ABSOLUTE MAXIMUM RATINGS**

Characteristic	Symbol	Notes	Rating	Units
Supply Voltage	V <sub>CC</sub>		8	V
Reverse Supply Voltage	V <sub>RCC</sub>		-0.1	V
Output Voltage	V <sub>IOUT</sub>		8	V
Reverse Output Voltage	V <sub>RIOUT</sub>		-0.1	V
Deinferend Inclotion Voltage	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	Pins 1-4 and 5-8; 60 Hz, 1 minute, T <sub>A</sub> =25°C	2100	VAC
Reinforced Isolation Voltage	V <sub>ISO</sub>	Maximum working voltage according to UL60950-1	184	$V_{peak}$
Pagia laglation Valtage	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	Pins 1-4 and 5-8; 60 Hz, 1 minute, T <sub>A</sub> =25°C	1500	VAC
Basic Isolation Voltage	V <sub>ISO(bsc)</sub>	Maximum working voltage according to UL60950-1	354	$V_{peak}$
Output Current Source	I <sub>OUT(Source)</sub>		3	mA
Output Current Sink	I <sub>OUT(Sink)</sub>		10	mA
Overcurrent Transient Tolerance	I <sub>P</sub>	1 pulse, 100 ms	100	Α
Nominal Operating Ambient Temperature	T <sub>A</sub>	Range E	-40 to 85	°C
Maximum Junction Temperature	T <sub>J</sub> (max)		165	°C
Storage Temperature	T <sub>stg</sub>		-65 to 170	°C

### **Isolation Characteristics**

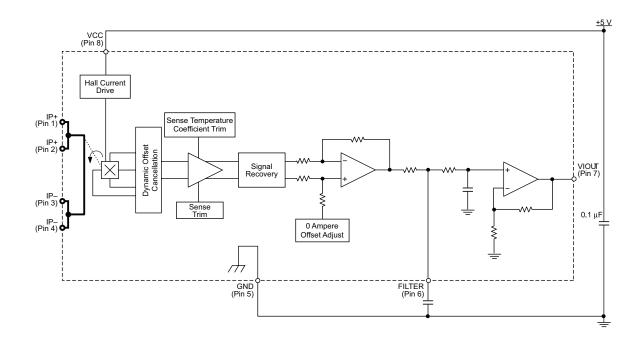
Characteristic Symbol		Notes	Rating	Unit
Dielectric Strength Test Voltage*	V <sub>ISO</sub>	Agency type-tested for 60 seconds per UL standard 60950-1, 1st Edition	2100	VAC
Working Voltage for Basic Isolation	V <sub>WFSI</sub>	For basic (single) isolation per UL standard 60950-1, 1st Edition	354	VDC or V <sub>pk</sub>
Working Voltage for Reinforced Isolation	V <sub>WFRI</sub>	For reinforced (double) isolation per UL standard 60950-1, 1st Edition	184	VDC or V <sub>pk</sub>

<sup>\*</sup> Allegro does not conduct 60-second testing. It is done only during the UL certification process.

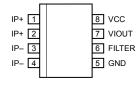
Parameter	Specification
Fire and Electric Shock	CAN/CSA-C22.2 No. 60950-1-03 UL 60950-1:2003; EN 60950-1:2001



### **FUNCTIONAL BLOCK DIAGRAM**



## **Pinout Diagram**



### **Terminal List**

Number	Name	Description
1 and 2	IP+	Input terminals for current being sampled; fused internally
3 and 4	IP-	Output terminals for current being sampled; fused internally
5	GND	Signal ground terminal
6	FILTER	Terminal for external capacitor that sets bandwidth
7	VIOUT	Analog output signal
8	VCC	Device power supply terminal



# Fully Integrated, Hall-Effect-Based Linear Current Sensor IC with 2.1 $kV_{RMS}$ Isolation and Low-Resistance Current Conductor

## COMMON OPERATING CHARACTERISTICS [1]: Over full range of T<sub>A</sub>, and V<sub>CC</sub> = 5 V, unless otherwise specified

Characteristic	Symbol	Test Conditions	Min.	Тур.	Max.	Units
ELECTRICAL CHARACTERIS	STICS					
Supply Voltage	V <sub>cc</sub>		4.5	5.0	5.5	V
Supply Current	I <sub>cc</sub>	V <sub>CC</sub> = 5.0 V, output open	-	10	13	mA
Output Capacitance Load	C <sub>LOAD</sub>	VIOUT to GND	-	-	10	nF
Output Resistive Load	R <sub>LOAD</sub>	VIOUT to GND	4.7	_	_	kΩ
Primary Conductor Resistance	R <sub>PRIMARY</sub>	T <sub>A</sub> = 25°C	_	1.2	_	mΩ
Rise Time	t <sub>r</sub>	$I_P = I_P(max), T_A = 25^{\circ}C, C_{OUT} = 10 \text{ nF}$	_	3.5	_	μs
Frequency Bandwidth	f	−3 dB, T <sub>A</sub> = 25°C; I <sub>P</sub> is 10 A peak-to-peak	_	80	_	kHz
Nonlinearity	E <sub>LIN</sub>	Over full range of I <sub>P</sub> , I <sub>P</sub> applied for 5 ms	-	±1.5	-	%
Zero Current Output Voltage	V <sub>IOUT(Q)</sub>	Unidirectional; I <sub>P</sub> = 0 A, T <sub>A</sub> = 25°C	-	V <sub>CC</sub> × 0.1	_	V
Power-On Time	t <sub>PO</sub>	Output reaches 90% of steady-state level, no capacitor on FILTER pin; T <sub>J</sub> =25; 20 A present on leadframe	_	35	_	μs
Magnetic Coupling [2]			_	12	_	G/A
Internal Filter Resistance [3]	R <sub>F(INT)</sub>			1.7		kΩ

<sup>[1]</sup> Device may be operated at higher primary current levels, I<sub>P</sub>, and ambient, T<sub>A</sub>, and internal leadframe temperatures, T<sub>A</sub>, provided that the Maximum Junction Temperature, T<sub>J</sub>(max), is not exceeded.

### **COMMON THERMAL CHARACTERISTICS** [1]

Characteristic	Symbol	Test Conditions	Min.	Тур.	Max.	Units
Operating Internal Leadframe Temperature	T <sub>A</sub>	E range	-40	_	85	°C
Characteristic	Symbol	Test Conditions			Value	Units
Junction-to-Lead Thermal Resistance [2] R <sub>BJL</sub> Mounted on the Allegro As		Mounted on the Allegro ASEK 713 evaluation board			5	°C/W
Junction-to-Ambient Thermal Resistance[2][3]	R <sub>θJA</sub>	Mounted on the Allegro 85-0322 evaluation board, incluconsumed by the board	udes the p	ower	23	°C/W

<sup>[1]</sup> Additional thermal information is available on the Allegro website.



<sup>[2] 1</sup>G = 0.1 mT.

 $<sup>^{[3]}\,</sup>R_{F(INT)}$  forms an RC circuit via the FILTER pin.

<sup>[2]</sup> The Allegro evaluation board has 1500 mm<sup>2</sup> of 2 oz. copper on each side, connected to pins 1 and 2, and to pins 3 and 4, with thermal vias connecting the layers. Performance values include the power consumed by the PCB. Further details on the board are available from the Frequently Asked Questions document on our website. Further information about board design and thermal performance also can be found in the Applications Information section of this datasheet.

<sup>[3]</sup> R<sub>0,JA</sub> values shown in this table are typical values, measured on the Allegro evaluation board. The actual thermal performance depends on the actual application board design, the airflow in the application, and thermal interactions between the device and surrounding components through the PCB and the ambient air. To improve thermal performance, see our applications material on the Allegro website.

# Fully Integrated, Hall-Effect-Based Linear Current Sensor IC with 2.1 $kV_{RMS}$ Isolation and Low-Resistance Current Conductor

## **x20A PERFORMANCE CHARACTERISTICS:** $T_A = -40$ °C to 85°C [1]; $V_{CC} = 5$ V, unless otherwise specified

Characteristic	Symbol	Test Conditions	Min.	Тур.	Max.	Units
Optimized Accuracy Range	Ι <sub>P</sub>		0	-	20	А
Sensitivity	Sens	Over full range of I <sub>P,</sub> T <sub>A</sub> = 25°C	178	185	190	mV/A
Noise	V <sub>NOISE(PP)</sub>	Peak-to-peak, $T_A$ = 25°C, 2 kHz external filter, 185 mV/A programmed Sensitivity, $C_F$ = 47 nF, $C_{OUT}$ = 10 nF, 2 kHz bandwidth	_	21	_	mV
Zero Current Output Slope	437	$T_A = -40$ °C to 25°C	_	0.08	_	mV/°C
Zero Current Output Slope	$\Delta V_{OUT(Q)}$	T <sub>A</sub> = 25°C to 150°C	_	0.16	_	mV/°C
Sensitivity Slope	ΛSens	$T_A = -40$ °C to 25°C	_	0.035	_	mV/A/°C
Sensitivity Slope	ΔSens	T <sub>A</sub> = 25°C to 150°C	-	0.019	-	mV/A/°C
Total Output Error [2]	E <sub>TOT</sub>	I <sub>P</sub> = 20 A, I <sub>P</sub> applied for 5 ms; T <sub>A</sub> = 25°C	_	±1.5	_	%

<sup>[1]</sup> Device may be operated at higher primary current levels, I<sub>P</sub>, and ambient temperatures, T<sub>A</sub>, provided that the Maximum Junction Temperature, T<sub>J</sub>(max), is not exceeded.

# **x30A PERFORMANCE** CHARACTERISTICS $T_A = -40^{\circ}C$ to $85^{\circ}C$ [1], $V_{CC} = 5$ V, unless otherwise specified

Characteristic	Symbol	Test Conditions	Min.	Тур.	Max.	Units
Optimized Accuracy Range	I <sub>P</sub>		0	_	30	А
Sensitivity	Sens	Over full range of I <sub>P,</sub> T <sub>A</sub> = 25°C	129	133	137	mV/A
Noise	V <sub>NOISE(PP)</sub>	Peak-to-peak, $T_A$ = 25°C, 2 kHz external filter, 133 mV/A programmed Sensitivity, $C_F$ = 47 nF, $C_{OUT}$ = 10 nF, 2 kHz bandwidth	_	15	_	mV
Zara Current Output Slane	rent Output Slope $\Delta V_{OUT(Q)}$	$T_A = -40$ °C to 25°C	_	0.06	_	mV/°C
Zero Current Output Slope		T <sub>A</sub> = 25°C to 150°C	_	0.1	_	mV/°C
Consitivity Clans	A.Como	$T_A = -40^{\circ}C \text{ to } 25^{\circ}C$	_	0.007	_	mV/A/°C
Sensitivity Slope	∆Sens	T <sub>A</sub> = 25°C to 150°C	_	-0.025	_	mV/A/°C
Total Output Error [2]	E <sub>TOT</sub>	I <sub>P</sub> = 30 A, I <sub>P</sub> applied for 5 ms; T <sub>A</sub> = 25°C	_	±1.5	_	%

<sup>[1]</sup> Device may be operated at higher primary current levels, I<sub>P</sub>, and ambient temperatures, T<sub>A</sub>, provided that the Maximum Junction Temperature, T<sub>J</sub>(max), is not exceeded.



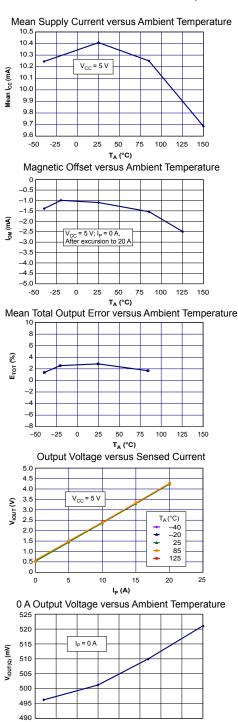
<sup>&</sup>lt;sup>[2]</sup> Percentage of  $I_P$ , with  $I_P$  = 20 A. Output filtered.

<sup>[2]</sup> Percentage of  $I_P$ , with  $I_P = 30$  A. Output filtered.

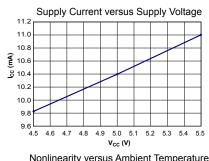
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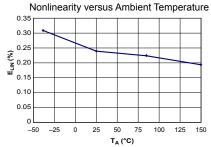
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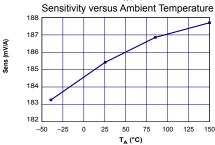
 $I_P = 20 A$ , unless otherwise specified

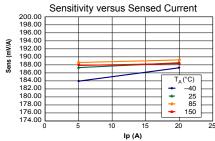


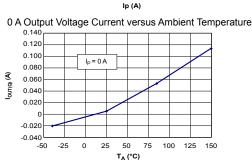
TA (°C)









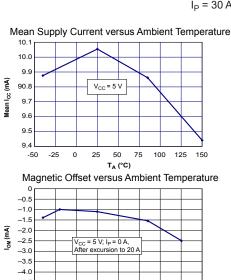


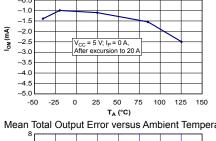


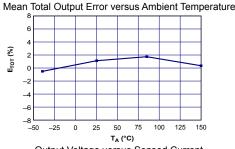
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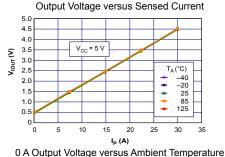
#### CHARACTERISTIC PERFORMANCE

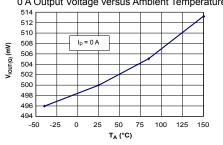
 $I_P = 30 A$ , unless otherwise specified

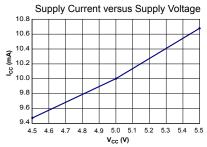


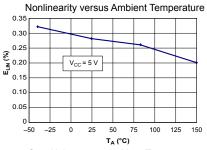


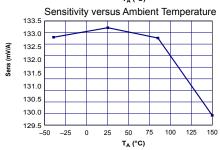


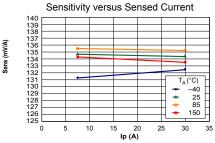


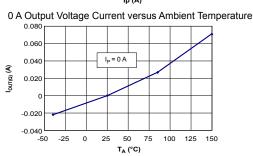












### **DEFINITIONS OF ACCURACY CHARACTERISTICS**

**Sensitivity (Sens).** The change in device output in response to a 1 A change through the primary conductor. The sensitivity is the product of the magnetic circuit sensitivity (G/A) and the linear IC amplifier gain (mV/G). The linear IC amplifier gain is programmed at the factory to optimize the sensitivity (mV/A) for the full-scale current of the device.

**Noise (V**<sub>NOISE</sub>). The product of the linear IC amplifier gain (mV/G) and the noise floor for the Allegro Hall effect linear IC ( $\approx$ 1 G). The noise floor is derived from the thermal and shot noise observed in Hall elements. Dividing the noise (mV) by the sensitivity (mV/A) provides the smallest current that the device is able to resolve.

**Linearity** ( $E_{LIN}$ ). The degree to which the voltage output from the IC varies in direct proportion to the primary current through its full-scale amplitude. Nonlinearity in the output can be attributed to the saturation of the flux concentrator approaching the full-scale current. The following equation is used to derive the linearity:

$$100 \left\{ 1 - \left[ \frac{(V_{\text{IOUT\_full-scale amperes}} - V_{\text{IOUT(Q)}})}{2 (V_{\text{IOUT\_half-scale amperes}} - V_{\text{IOUT(Q)}})} \right] \right\}$$

where  $V_{IOUT\_full\text{-scale amperes}}$  = the output voltage (V) when the sampled current approximates full-scale  $\pm I_P$ .

Quiescent output voltage ( $V_{IOUT(Q)}$ ). The output of the device when the primary current is zero. For a unipolar supply voltage, it nominally remains at  $V_{CC} \times 0.1$ . Thus,  $V_{CC} = 5$  V translates into  $V_{IOUT(Q)} = 0.5$  V. Variation in  $V_{IOUT(Q)}$  can be attributed to the resolution of the Allegro linear IC quiescent voltage trim and thermal drift.

Electrical offset voltage ( $V_{OE}$ ). The deviation of the device output from its ideal quiescent value of  $V_{CC} \times 0.1$  due to nonmagnetic causes. To convert this voltage to amperes, divide by the device sensitivity, Sens.

Accuracy ( $E_{TOT}$ ). The accuracy represents the maximum deviation of the actual output from its ideal value. This is also known as the total output error. The accuracy is illustrated graphically in the output voltage versus current chart at right.

Accuracy is divided into four areas:

- **0** A at **25°C**. Accuracy at the zero current flow at 25°C, without the effects of temperature.
- 0 A over Δ temperature. Accuracy at the zero current flow including temperature effects.
- Full-scale current at 25°C. Accuracy at the full-scale current at 25°C, without the effects of temperature.
- Full-scale current over Δ temperature. Accuracy at the full-scale current flow including temperature effects.

**Ratiometry**. The ratiometric feature means that its 0 A output,  $V_{IOUT(Q)}$ , (nominally equal to  $V_{CC} \times 0.1$ ) and sensitivity, Sens, are proportional to its supply voltage,  $V_{CC}$ . The following formula is used to derive the ratiometric change in 0 A output voltage,  $\Delta V_{IOUT(O)RAT}$  (%).

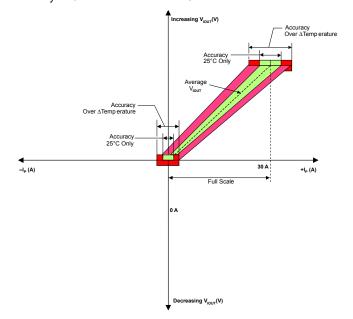
$$100 \left( \frac{V_{\text{IOUT(Q)VCC}} / V_{\text{IOUT(Q)5V}}}{V_{\text{CC}} / 5 \text{ V}} \right)$$

The ratiometric change in sensitivity,  $\Delta Sens_{RAT}$  (%), is defined as:

$$100 \left( \frac{Sens_{VCC} / Sens_{5V}}{V_{CC} / 5 V} \right)$$

## **Output Voltage versus Sampled Current**

Accuracy at 0 A and at Full-Scale Current



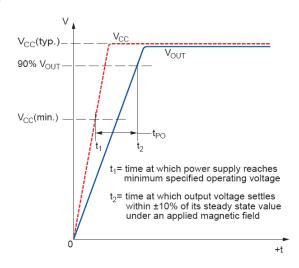


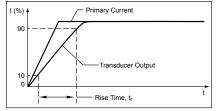
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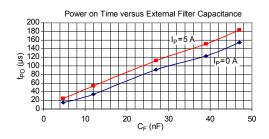
## **Definitions of Dynamic Response Characteristics**

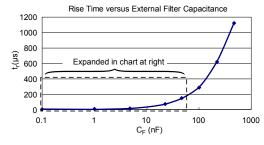
**Power-On Time**  $(t_{PO})$ . When the supply is ramped to its operating voltage, the device requires a finite time to power its internal components before responding to an input magnetic field. Power-On Time, t<sub>PO</sub>, is defined as the time it takes for the output voltage to settle within  $\pm 10\%$  of its steady state value under an applied magnetic field, after the power supply has reached its minimum specified operating voltage, V<sub>CC</sub>(min), as shown in the chart at right.

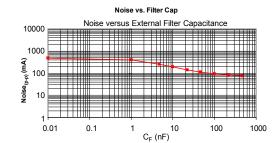
Rise time  $(t_r)$ . The time interval between a) when the device reaches 10% of its full-scale value, and b) when it reaches 90% of its full scale value. The rise time to a step response is used to derive the bandwidth of the device, in which  $f(-3 \text{ dB}) = 0.35/t_r$ . Both t<sub>r</sub> and t<sub>RESPONSE</sub> are detrimentally affected by eddy current losses observed in the conductive IC ground plane.

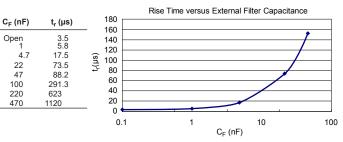












Open 1

22

47

220

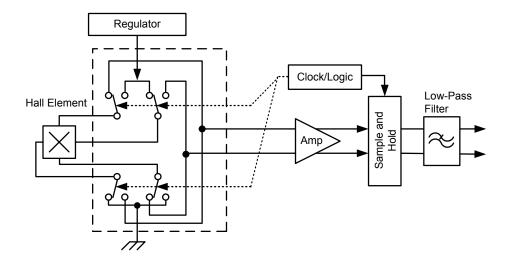
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## CHOPPER STABILIZATION TECHNIQUE

Chopper Stabilization is an innovative circuit technique that is used to minimize the offset voltage of a Hall element and an associated on-chip amplifier. Allegro has a Chopper Stabilization technique that nearly eliminates Hall IC output drift induced by temperature or package stress effects. This offset reduction technique is based on a signal modulation-demodulation process. Modulation is used to separate the undesired DC offset signal from the magnetically induced signal in the frequency domain. Then, using a low-pass filter, the modulated DC offset is suppressed while the magnetically induced signal passes through

the filter. As a result of this chopper stabilization approach, the output voltage from the Hall IC is desensitized to the effects of temperature and mechanical stress. This technique produces devices that have an extremely stable Electrical Offset Voltage, are immune to thermal stress, and have precise recoverability after temperature cycling.

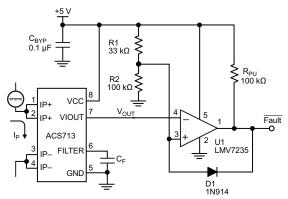
This technique is made possible through the use of a BiCMOS process that allows the use of low-offset and low-noise amplifiers in combination with high-density logic integration and sample and hold circuits.



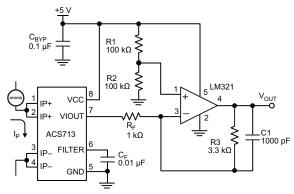
Concept of Chopper Stabilization Technique



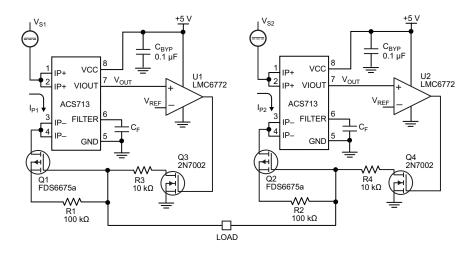
## **TYPICAL APPLICATIONS**



Application 2. 10 A Overcurrent Fault Latch. Fault threshold set by R1 and R2. This circuit latches an overcurrent fault and holds it until the 5 V rail is powered down.



Application 3. This configuration increases gain to 610 mV/A (tested using the ACS712ELC-05A).



Application 4. Control circuit for MOSFET ORing.



### IMPROVING SENSING SYSTEM ACCURACY USING THE FILTER PIN

In low-frequency sensing applications, it is often advantageous to add a simple RC filter to the output of the device. Such a low-pass filter improves the signal-to-noise ratio, and therefore the resolution, of the device output signal. However, the addition of an RC filter to the output of a sensor IC can result in undesirable device output attenuation — even for DC signals.

Signal attenuation,  $\Delta V_{ATT}$ , is a result of the resistive divider effect between the resistance of the external filter,  $R_F$  (see Application 5), and the input impedance and resistance of the customer interface circuit,  $R_{INTFC}$ . The transfer function of this resistive divider is given by:

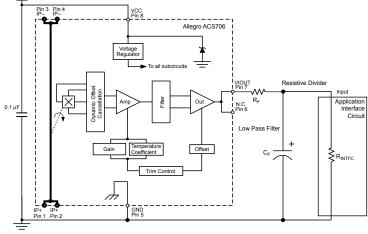
 $\Delta V_{\text{ATT}} = V_{\text{IOUT}} \left( \frac{R_{\text{INTFC}}}{R_{\text{F}} + R_{\text{INTFC}}} \right) \quad .$ 

Even if R<sub>F</sub> and R<sub>INTFC</sub> are designed to match, the two individual resistance values will most likely drift by different amounts over

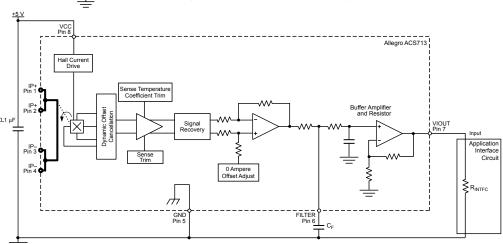
temperature. Therefore, signal attenuation will vary as a function of temperature. Note that, in many cases, the input impedance,  $R_{\rm INTFC}$ , of a typical analog-to-digital converter (ADC) can be as low as  $10~{\rm k}\Omega$ .

The ACS713 contains an internal resistor, a FILTER pin connection to the printed circuit board, and an internal buffer amplifier. With this circuit architecture, users can implement a simple RC filter via the addition of a capacitor,  $C_F$  (see Application 6) from the FILTER pin to ground. The buffer amplifier inside of the ACS713 (located after the internal resistor and FILTER pin connection) eliminates the attenuation caused by the resistive divider effect described in the equation for  $\Delta V_{ATT}$ . Therefore, the ACS713 device is ideal for use in high-accuracy applications that cannot afford the signal attenuation associated with the use of an external RC low-pass filter.

Application 5. When a low pass filter is constructed externally to a standard Hall effect device, a resistive divider may exist between the filter resistor,  $R_{\text{F}}$ , and the resistance of the customer interface circuit,  $R_{\text{INTFC}}$ . This resistive divider will cause excessive attenuation, as given by the transfer function for  $\Delta V_{\text{ATT}}$ .



Application 6. Using the FILTER pin provided on the ACS713 eliminates the attenuation effects of the resistor divider between  $R_{\text{F}}$  and  $R_{\text{INTFC}}$ , shown in Application 5.

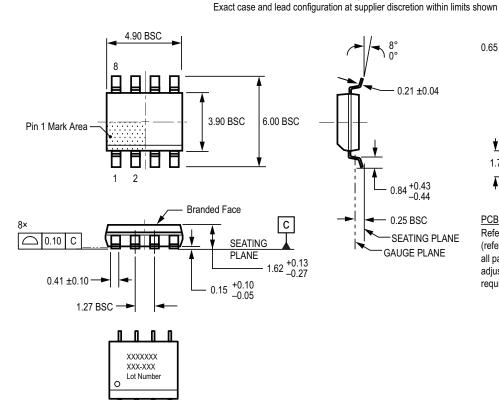


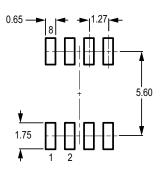
# Fully Integrated, Hall-Effect-Based Linear Current Sensor IC with 2.1 $kV_{RMS}$ Isolation and Low-Resistance Current Conductor

## Package LC, 8-pin SOIC

### For Reference Only; not for tooling use

(reference Allegro DWG-0000385, Rev. 2 or JEDEC MS-012AA)
Dimensions in millimeters – Not to scale
Dimensions exclusive of mold flash, gate burrs, and dambar protrusions





PCB Layout Reference View
Reference land pattern layout
(reference IPC7351 SOIC127P600X175-8M);
all pads a minimum of 0.20 mm from all adjacent pads;
adjust as necessary to meet application process
requirements and PCB layout tolerances.

Standard Branding Reference View

Lines 1, 2 = 8 characters Line 3 = 5 characters

Line 1: Part Number Line 2: Temp, Pkg - Amps

Line 3: First 5 Characters of Assembly Lot Number

Belly Brand: Country of Origin, Lot Number

Branding scale and appearance at supplier discretion



# Fully Integrated, Hall-Effect-Based Linear Current Sensor IC with 2.1 $kV_{RMS}$ Isolation and Low-Resistance Current Conductor

### **Revision History**

Number	Date	Description
12	November 16, 2012	Update rise time and isolation, I <sub>OUT</sub> reference data, patents
13	June 5, 2017	Updated product status
14	December 10, 2018	Updated certificate numbers
15	May 17, 2019	Updated TUV certificate mark and minor editorial updates
16	January 30, 2020	Updated product status and minor editorial updates
17	February 7, 2022	Updated package drawing (page 13)
18	February 8, 2023	Updated selection guide heading (page 2)

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